

# User's manual and Technical description

Self-Powered Feeder Protection

REJ603



**ABB**





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## Conformity

This product complies with the directive of the Council of the European Communities on the approximation of the laws of the Member States relating to electromagnetic compatibility (EMC Council Directive 2004/108/EC) and concerning electrical equipment for use within specified voltage limits (Low-voltage directive 2006/95/EC). This conformity is the result of a test conducted by ABB in accordance with Article 10 of the directive in agreement with the product standards EN 50263 and EN 60255-26 for the EMC directive, and with the product standards EN 60255-6 and EN 60255-27 for the low voltage directive. The IED is designed in accordance with the international standards of the IEC 60255 series. are hereby required to ensure that all measures are taken to exclude or mitigate such risks.

## Safety information



Dangerous voltages can occur on the connectors, even though the auxiliary voltage has been disconnected.



Non-observance can result in death, personal injury or substantial property damage.



Only a competent electrician is allowed to carry out the electrical installation.



National and local electrical safety regulations must always be followed.



The terminals meant for connection to earth must be carefully earthed.



Removal of the equipment panel cover may expose live parts which may contain high voltage potential and touching these may cause personal injury.



The device contains components which are sensitive to electrostatic discharge. Unnecessary touching of electronic components must therefore be avoided.



On removal of terminal connectors for current transformer, there is no automatic CT shorting provision. Do not open the secondary of a live CT since dangerous voltage can occur on the terminal connectors. For safety, secondary of live CT must be shorted before opening terminal connectors.



Breaking the sealing tape on the top rear side of the device will result in loss of warranty and proper operation will no longer be guaranteed.

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## **Section 1      Introduction**

### **1.1                      About this manual**

This manual provides basic information on the protection relay REJ603 and presents detailed instructions on how to use the relay. In addition to the instructive part, a short chapter on commissioning of the relay is included.

### **1.2                      The use of the relay**

REJ603 is a feeder protection relay mainly designed for the selective short-circuit and earth fault protection of feeders in secondary distribution networks and for protection of transformers in utilities and industries.

REJ603 is a CT-powered protection relay and based on a microprocessor environment. The relay is used in combination with special ring type current transformer. REJ603 relay in combination with circuit breaker can replace the combination of load breaker switch with HV fuses. Thereby providing more improved protection for growing power distribution networks.

### **1.3                      Guarantee**

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## 1.4 Safety indication symbols

This publication includes the following icons that point out safety-related conditions or other important information:



The electrical warning icon indicates the presence of a hazard which could result in electrical shock.



The warning icon indicates the presence of a hazard which could result in personal injury.



The caution icon indicates important information or warning related

Although warning hazards are related to personal injury, it should be understood that operation of damaged equipment could, under certain operation conditions, result in degraded process performance leading to personal injury or death. Therefore, comply fully with all warning and caution notices.

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## Section 2 REJ603 overview

### 2.1 Relay application

REJ603 relay is intended to be used for the selective short-circuit and earth-fault protection of feeders in secondary distribution networks and for protection of transformers in utilities and industries. The relay is a self-powered Numerical relay, which does not require external auxiliary supply voltage, making it an ideal choice for installation even in remote locations where auxiliary supplies are not available. The relay derives power for its operation from the current transformers. REJ603 is primarily used in Ring Main Units (RMU) within distribution network.

Relay provides earth current measurement through internal calculation or has the provision for measuring it from the external core balance current transformer (CBCT).

The key features of the relay are

- Self-powered three phase non-directional overcurrent and earth-fault protection with DMT and IDMT characteristics
- Dual mode of earth fault measurement - internal vector summation or external CBCT input
- Integrated IDMT curves (IEC and Special) in a single product to cover time coordination needs of secondary distribution protection
- Protection blocking by second harmonic measurement for stability during magnetizing inrush of transformers
- Capacitor discharge impulse output for low energy trip coil
- Built-in hand-reset electromechanical Flag for trip indication
- Easy setting by DIP switches, protected by a transparent cover
- Compact design and mounting arrangement suitable for Ring Main Unit (RMU) applications
- Test facility for testing entire scheme including primary CT, relay, and trip coil

## 2.2 Product version history

Product version	Release date	Product history
1.0	18.03.2008	Product released

## 2.3 Protection functionality

Protection	IEC	ANSI
Three phase overcurrent protection, low-set stage	3I>	51
Three phase overcurrent protection, high-set stage	3I>>	50 / 51
Earth-fault protection, low-set stage	I <sub>0</sub> >	51N
Earth-fault protection, high-set stage	I <sub>0</sub> >>	50N / 51N
Three phase transformer inrush detector	3I <sub>2f</sub> >	68

## 2.4 Description of operation

The combined overcurrent and earth-fault relay is a secondary relay to be connected to the current transformers of the protected object. Apart from the measurement (inputs), the relay derives energy required for its own operation and tripping of circuit breaker from the current transformers. There are two LED's on the front panel. When minimum current required for operation is available the green 'Ready' LED glows indicating the relay is in operation. On detection of a fault the relay trips the circuit breaker in accordance with the settings. The relay also does internal health check at regular interval and intimates user in case of any internal relay failure. The internal relay failure is indicated by red 'IRF' LED. .

When the phase current exceeds the set operate time at definite time operation or the calculated operate time at inverse time operation elapses, the overcurrent unit operates. In the same way the high-set stage I>> of the overcurrent unit operates when the set operate time elapses.

When the earth-fault current exceeds the set operate time at definite time operation or the calculated operate time at inverse time operation elapses, the earth-fault unit operates. In the same way the high-set stage I<sub>0</sub>>> of the earth-fault unit operates when the set operate time elapses.

The low-set stage of the overcurrent unit and the low-set stage of the earth-fault unit may be given definite time or inverse definite minimum time (IDMT) characteristic. When the IDMT characteristic is chosen, four standard and three special time/current curves are available. The standard curves comply with the BS142 and IEC 60255 and are named Normal inverse, Very inverse, Extremely inverse, Long-time inverse. Three special curves namely RI-curve, HR Fuse curve, and FR Fuse curve are also provided.

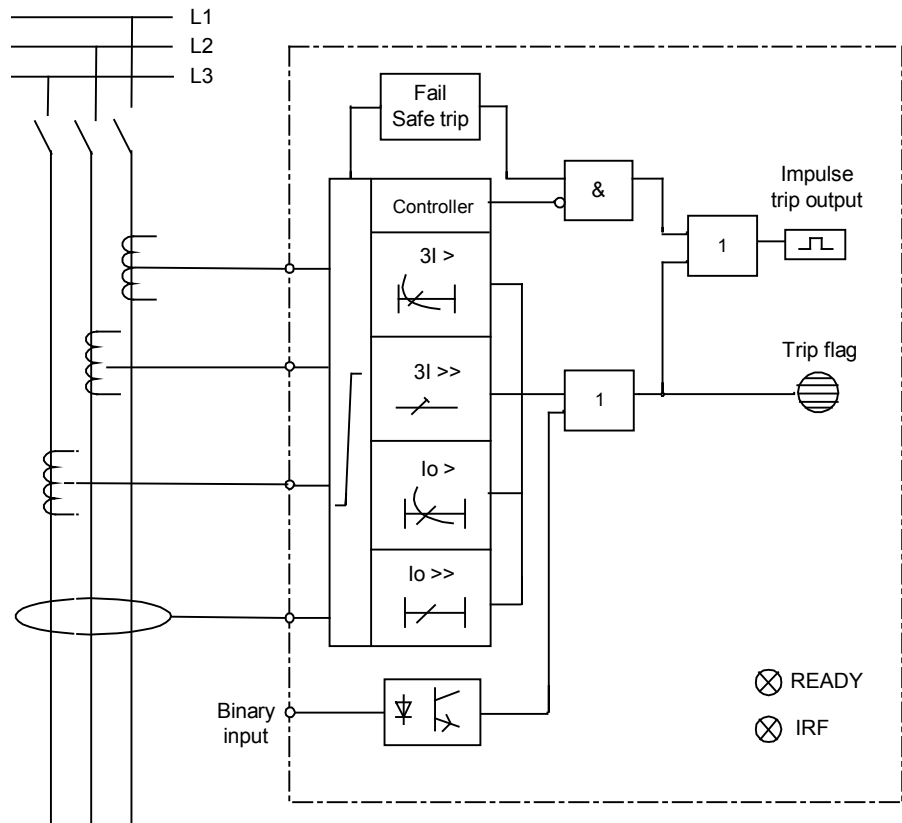


Fig. 1 – Block diagram of self-powered feeder protection relay REJ603

When overcurrent or earth-fault unit operates, the relay issues a ‘trip’ command in the form of a low energy impulse to the shunt trip coil of breaker. A mechanical flag ‘Trip’ turns red when the relay operates. The flag can only be reset manually when the relay is energized and the ‘Trip’ flag turns green after reset. The relay includes one external binary input, which is controlled by an external control voltage (24-240 V AC/DC). This input can be utilized to give an output trip command.

In case of controller failure, the relay would offer short circuit protection for currents greater than 20\*Is maximum. Such a redundancy is achieved through intelligent hardware.

There are three possible ways to give an output trip command as shown in figure2.

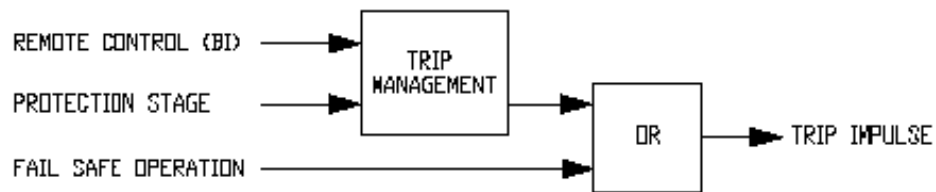


Fig. 2 – Output trip arrangement for REJ603

The protection system, comprising of, CT’s, relay and low-energy trip-coil can be tested for its integrity by using the test winding of the current transformer, which is brought into the relay test terminals.

For deriving the operational power, the relay requires minimum current flow of 0.9 times the minimum setting current “Ismin” in at least one phase or 0.4 times the minimum setting current “Ismin” in all three phases.

output trip command as shown in figure2.

CT Type: (Ismin –Ismax)	Min. current required in any one phase for relay operation	Min. current required in three phase for relay operation
REJ603-CT2: 16A–56A	14.4A	6.4A
REJ603-CT3: 32A–112A	28.8A	12.8A
REJ603-CT4: 64A–224A	57.6A	25.6A
REJ603-CT5: 128A–448A	115.2A	51.2A

## Section 3 Technical data

### 3.1 Dimensions

Width	96 mm
Height	160 mm
Depth	149 mm
Weight	~ 0.8 kg

### 3.2 Energizing Inputs

Rated Frequency		50/60 Hz ± 5 Hz
Phase inputs	Nominal primary current	
	CT type	Rated CT current range $I_s$
	REJ603-CT2	16 - 56 A
	REJ603-CT3	32 - 112 A
	REJ603-CT4	64 - 224 A
	REJ603-CT5	128 - 448 A
	Thermal withstand capability	
<ul style="list-style-type: none"> <li>Continuously</li> <li>For 1 s</li> <li>For 3 s</li> </ul>	$2.5 \times I_{smax}$ 25 kA primary current 20 kA primary current	
Dynamic current withstand:		
<ul style="list-style-type: none"> <li>Half-wave value</li> </ul>	62.5 kA primary current	
Earth input	Rated current, $I_n$	1 A
	Thermal withstand capability	
	<ul style="list-style-type: none"> <li>Continuously</li> <li>For 1 s</li> <li>For 3 s</li> </ul>	4 A 100 A
	Dynamic current withstand:	
	<ul style="list-style-type: none"> <li>Half-wave value</li> </ul>	250 A
Input impedance		< 100 mΩ

### 3.3 Binary inputs

Rated voltage	24 - 240 V AC/DC
Operating range	-15%...+10% for AC , -30% ... +20% for DC
Current drain	2...15 mA
Power consumption	< 0.8 W

### 3.4 Impulse voltage trip output

Rated output voltage	12 V
Pulse time	30 ms
Energy	50 mJ

## 3.5

## Setting range and accuracy

Setting range of nominal current  $I_s$ 

REJ603-CT2	16	18	20	22	24	26	28	30	32	34	36	40	44	48	52	56
REJ603-CT3	32	36	40	44	48	52	56	60	64	68	72	80	88	96	104	112
REJ603-CT4	64	72	80	88	96	104	112	120	128	136	144	160	176	192	208	224
REJ603-CT5	128	144	160	176	192	208	224	240	256	272	288	320	352	384	416	448

## Low-set phase over-current protection stage I&gt;

Measuring range	$0.9 \times I_{smin} \dots 20 \times I_{smax}$
Setting range of pick-up current I >	$0.9 \dots 2.5 \times I_s$
Setting resolution/steps	$I_s \times 0.9 \dots 2.5$ (31 steps), exit
Accuracy of pick-up current	$\pm 5.0\%$ of set value in the temperature range 0...70°C $\pm 7.5\%$ of set value in the temperature range -40...85°C
Setting range of definite time delay t >	0.05...3.0 sec
Setting resolution/steps	0.05, 0.07, 0.1, 0.15, 0.2, 0.25, 0.3, 0.4, 0.6, 0.8, 1.0, 1.4, 1.8, 2.2, 2.6, 3.0
Accuracy of operate time	$\pm 1\%$ or 10 ms, whichever is greater
Setting of inverse time characteristics	<b>IEC 60255-3:</b> Normal Inverse, Very Inverse, Extremely Inverse, Long time Inverse <b>Special Curves:</b> RI Inverse Time, HR-Fuse, FR-Fuse
Setting range of time multiplier k	0.05...3.0
Setting resolution/steps	0.05, 0.07, 0.1, 0.15, 0.2, 0.25, 0.3, 0.4, 0.6, 0.8, 1.0, 1.4, 1.8, 2.2, 2.6, 3.0
Accuracy of operate time IEC characteristics RI characteristics HR, FR curve characteristics	class E(5) $\pm 35$ ms, whichever is greater As per NI (IEC) curve $\pm 20\%$ of set value or $\pm 35$ ms, whichever is greater

## High-set phase overcurrent protection stage I&gt;&gt;

Setting range of pick-up current I>>	$1 \dots 20 \times I_s$
Setting resolution/steps	$I_s \times 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 12, 14, 16, 18, 20$ , exit
Accuracy of pick-up current	$\pm 5\%$ of set value in the temperature range 0...70°C $\pm 7.5\%$ of set value in the temperature range -40...85°C

Setting range of definite time delay $t_{>>}$	0.04...3.0 sec
Setting resolution/steps	0.04, 0.07, 0.1, 0.15, 0.2, 0.25, 0.3, 0.4, 0.6, 0.8, 1.0, 1.4, 1.8, 2.2, 2.6, 3.0
Accuracy of Operate time	$\pm 1\%$ or 10 ms, whichever is greater

<b>Low-set earth-fault protection stage <math>I_0&gt;</math></b>	
Nominal value of earth current • Internal measurement • External measurement	$I_s$ $I_n: 1 \text{ A}$
Measurement range	$0.9 \times I_{smin} \dots 20 \times I_{smax} / 0.1 \dots 20 \times I_n$
Setting range of pick-up current $I_0>$	$0.1 \dots 1 \times I_s / 0.1 - 1 \times I_n$
Setting resolution/steps	$I_s$ or $I_n \times 0.1 \dots 1.0$ (31 steps), exit
Accuracy of pick-up current Internal measurement  External measurement	$\pm 3\%$ of $I_s$ in the temperature range $0 \dots 70^\circ\text{C}$ $\pm 7.5\%$ of $I_s$ in the temperature range $-40 \dots 85^\circ\text{C}$ $\pm 5\%$ of $I_n$ in the temperature range $0 \dots 70^\circ\text{C}$ $\pm 20\%$ of $I_n$ in the temperature range $-40 \dots 85^\circ\text{C}$
Setting range of definite time delay $t_0>$	0.05...3.0 sec
Setting resolution/steps	0.05, 0.07, 0.1, 0.15, 0.2, 0.25, 0.3, 0.4, 0.6, 0.8, 1.0, 1.4, 1.8, 2.2, 2.6, 3.0
Accuracy of operate time	$\pm 1\%$ or 10 ms, whichever is greater
Setting of inverse time characteristics	<b>IEC 60255-3:</b> Normal Inverse, Very Inverse Extremely Inverse, Long time Inverse <b>Special Curves:</b> RI Inverse Time, HR-Fuse, FR-Fuse
Setting range of time multiplier $k_0$	0.05...3.0
Setting resolution/steps	0.05, 0.07, 0.1, 0.15, 0.2, 0.25, 0.3, 0.4, 0.6, 0.8, 1.0, 1.4, 1.8, 2.2, 2.6, 3.0
Accuracy of operate time IEC characteristics RI characteristics HR, FR curve characteristics	class E(5) $\pm 35$ ms, whichever is greater As per NI (IEC) curve $\pm 20\%$ of set value or $\pm 35$ ms, whichever is greater

<b>High-set earth-fault protection stage I<sub>0</sub>&gt;&gt;</b>	
Setting range of pick-up current I <sub>0</sub> >>	1...20 x I <sub>s</sub> / 1...20 x I <sub>n</sub>
Setting resolution/steps	I <sub>s</sub> or I <sub>n</sub> x 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 12, 14, 16, 18, 20, exit
Accuracy of pick-up current Internal measurement	±3% of set value in the temperature range 0...70°C
External measurement	±7.5% of set value in the temperature range -40...85°C ±5% of set value in the temperature range 0...70°C ±15% of set value in the temperature range -40...85°C
Setting range of definite time delay t <sub>0</sub> >>	0.04...3.0 sec
Setting resolution/steps	0.04, 0.07, 0.1, 0.15, 0.2, 0.25, 0.3, 0.4, 0.6, 0.8, 1.0, 1.4, 1.8, 2.2, 2.6, 3.0
Accuracy of operate time	±1% or 10 ms which ever is greater

### 3.6 Degree of protection by enclosure

Front portion with cover	IP 54
Side with connection terminals	IP 20

### 3.7 Environmental conditions and test

<b>Environmental conditions</b>	
Service temperature range	-40...+85°C
Relative humidity	< 93%
Atmospheric pressure	86...106 kPa
Altitude	up to 2000 m
Transport and storage temperature range	-40...+85°C

<b>Environmental tests</b>	
Dry heat test	According to IEC 60068-2-2 Test values: • 16 h at +70°C • 96 h at +85°C
Dry cold test	According to IEC 60068-2-1 Test values: • 16 h at -25°C • 96 h at -40°C
Damp heat test, cyclic	According to IEC 60068-2-30 Test values: • 2 cycles at +25...55°C humidity 95...97%
Damp heat test, steady state	According to IEC 60068-2-78 Test values: • 96 h at +40°C humidity 94%
Storage test	According to IEC 60068-2-8 Test values: • 96 h at +85°C • 96 h at -40°C

<b>Electromagnetic compatibility tests</b>	
The EMC immunity test level meets the requirements listed below:	
1 MHz burst disturbance test • Common mode • Differential mode	According to IEC 61000-4-12 and IEC 60255-22-1 2.0KV, 1MHz, 400 pulses/sec 1.0KV, 1MHz, 400 pulses/sec
Electrostatic discharge test • Contact discharge • Air discharge	According to IEC 60255-22-2, class III, 6kV, 150 pF/330 Ω 8kV, 150 pF/330 Ω
Radiated, electro-magnetic field immunity test	According to IEC 60255-22-3, level III, Test values: 10 V/m, f = 80...1000 MHz

## Section 4 Protection characteristics

### 4.1 Time / Current characteristics

REJ603 relay has two-stage low-set and high-set non-directional overcurrent and earth-fault protection stages. The relay supports Definite time and IDMT characteristics for both phase and earth-fault protection. The operation of the low-set overcurrent stage I> and the low-set earth-fault stage IO> is based on definite time or inverse time characteristic, as selected by the user. The high-set stage has instantaneous and definite time characteristics.

When IDMT characteristic has been selected, the operating time of the stage will be a function of the current; the higher the current, the shorter the operating time. The stage includes seven time/current curve sets – four according to the BS 142 and IEC 60255 standards namely normal inverse, very inverse, extremely inverse and long-time inverse and three special curves, named RI type curve, HR fuse curve and FR fuse curve.

#### 4.1.1 IEC characteristics

The relationship between current and time for standard normal inverse, very inverse, extremely inverse and long-time inverse complies with the BS 142:1966 and IEC 60255-3 standards and can be expressed as follows:

$$t = \frac{K * \beta}{\left(\frac{I}{I_{set}}\right)^\alpha - 1}$$

where,

$t$  = operate time in seconds

$K$  = time multiplier

$I$  = measured current value

$I_{set}$  = set start current value

The slope of the time/current characteristics shall be determined by the constants  $\alpha$  and  $\beta$  as indicated below:

Slope of the time/current curve set	$\alpha$	$\beta$
Normal inverse	0.02	0.14
Very inverse	1.0	13.5
Extremely inverse	2.0	80.0
Long time inverse	1.0	120.0

### 4.1.2 RI type characteristics

The RI-type characteristic is a special characteristic used mainly in combination with existing mechanical relays. The characteristic is based on the following mathematical expression:

$$t = \frac{K}{\alpha - \beta(I/I_{set})}$$

where,

$t$  = operate time in seconds

$K$  = time multiplier

$I$  = measured current value

$I_{set}$  = set start current value

$\alpha$  = 0.339

$\beta$  = 0.236

### 4.1.3 HR Fuse and FR Fuse type characteristics

The HR and FR Fuse type characteristic is a special characteristic used mainly in combination with fuses. The characteristic is based on the following mathematical expression:

HR Fuse type characteristic is based on the following mathematical expression:

$$t = 10^{\frac{(\log(2 * (I / I_{set}) * (-3.832) + 3.66))}{\alpha / 0.1}}$$

FR Fuse type characteristic is based on the following mathematical expression:

$$t = 10^{\frac{(\log(I / I_{set}) * (-7.16) + 3.0)}{\alpha / 0.1}} \text{ for } I/I_{set} = 1-2$$

$$t = 10^{\frac{(\log(I / I_{set}) * (-5.4) + 2.47)}{\alpha / 0.1}} \text{ for } I/I_{set} = 2-2.66$$

$$t = 10^{\frac{(\log(I / I_{set}) * (-4.24) + 1.98)}{\alpha / 0.1}} \text{ for } I/I_{set} > 2.66$$

### 4.1.4 Normal inverse-time characteristics curve

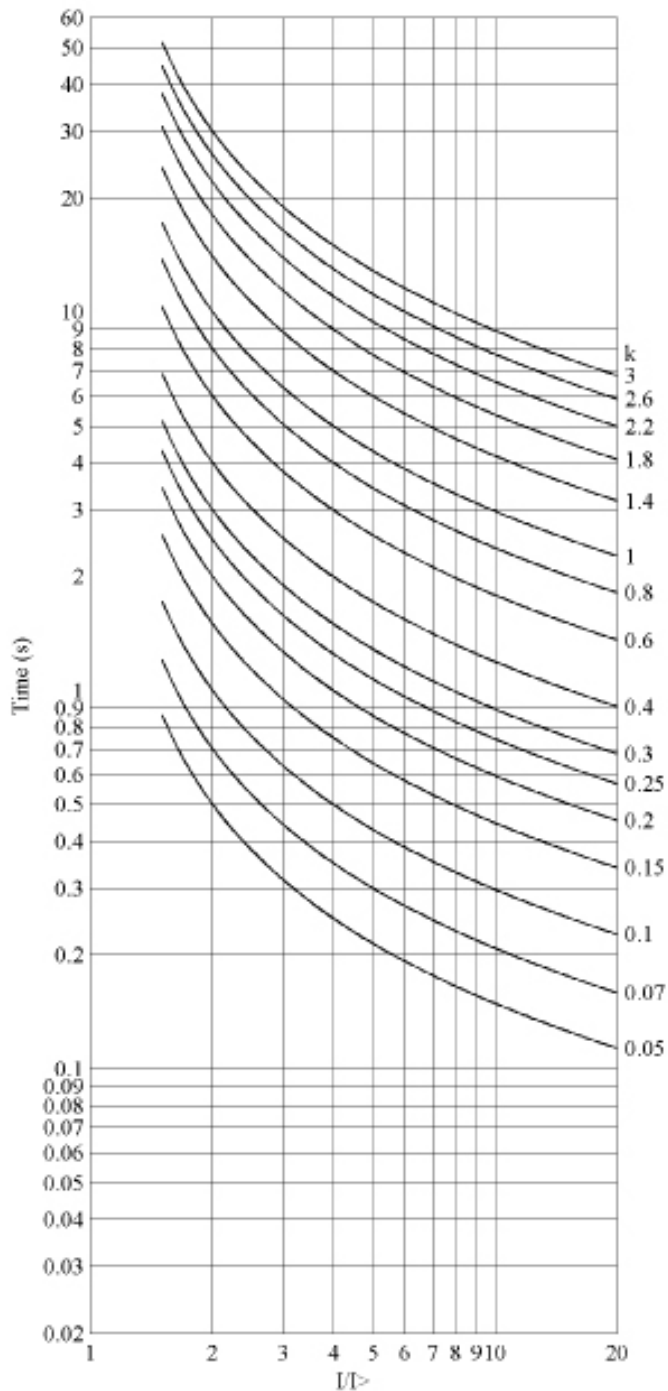


Fig. 3 – Normal inverse-time characteristics of relay REJ603

### 4.1.5 Extremely inverse-time characteristics

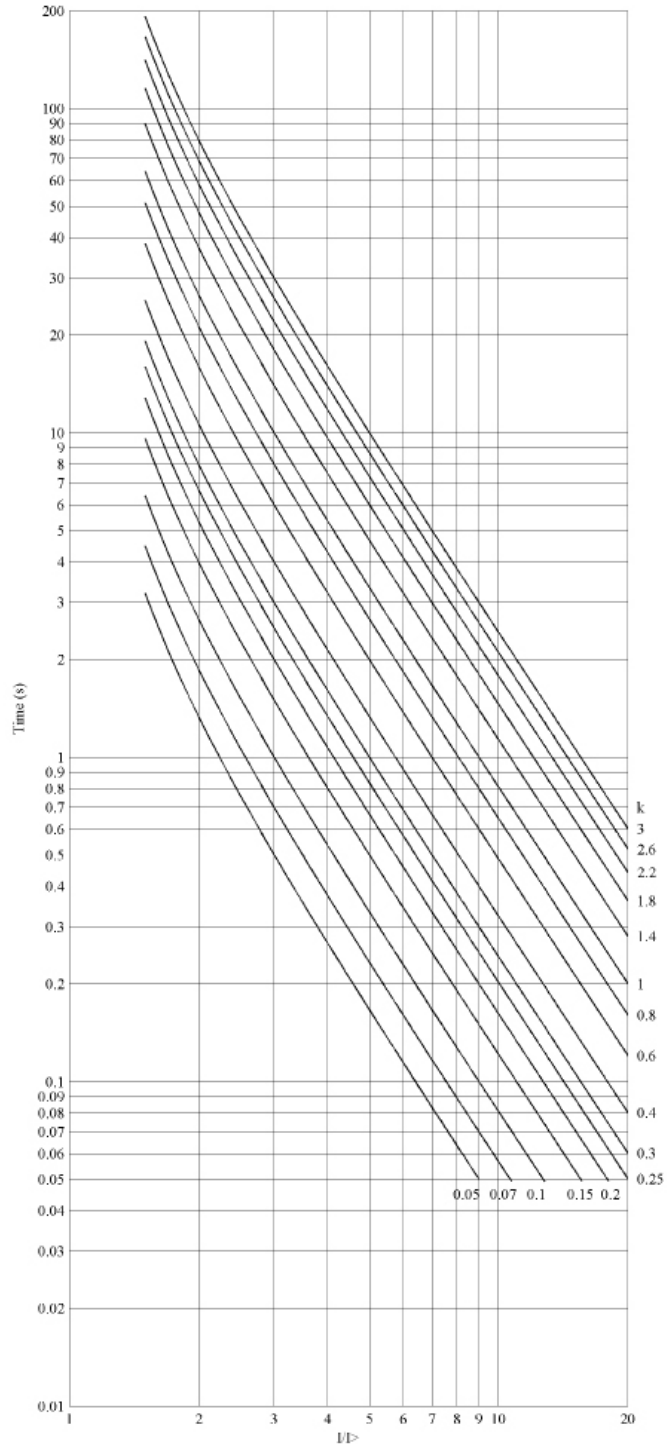


Fig. 4 – Extremely inverse-time characteristics of relay REJ603

### 4.1.6 Very inverse-time characteristics curve

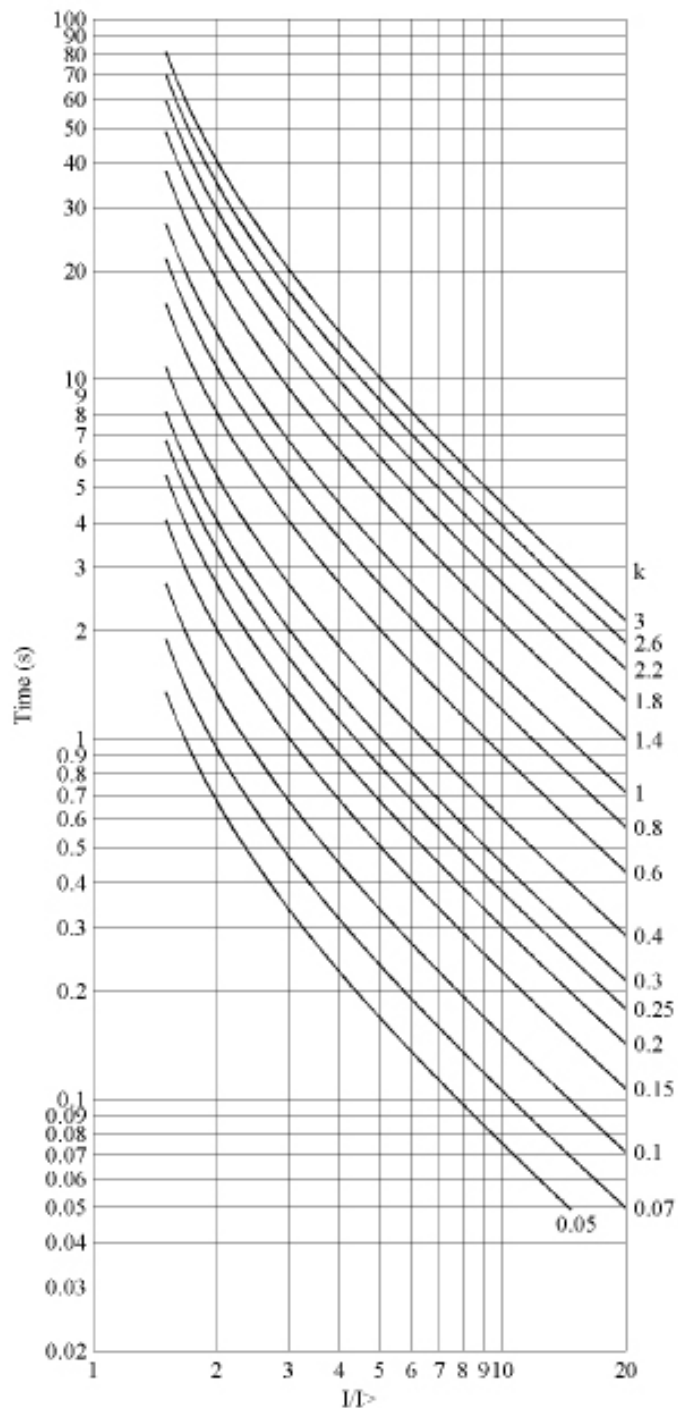


Fig. 5 – Very inverse-time characteristics of relay REJ603

### 4.1.7 Long-time inverse-time characteristics curve

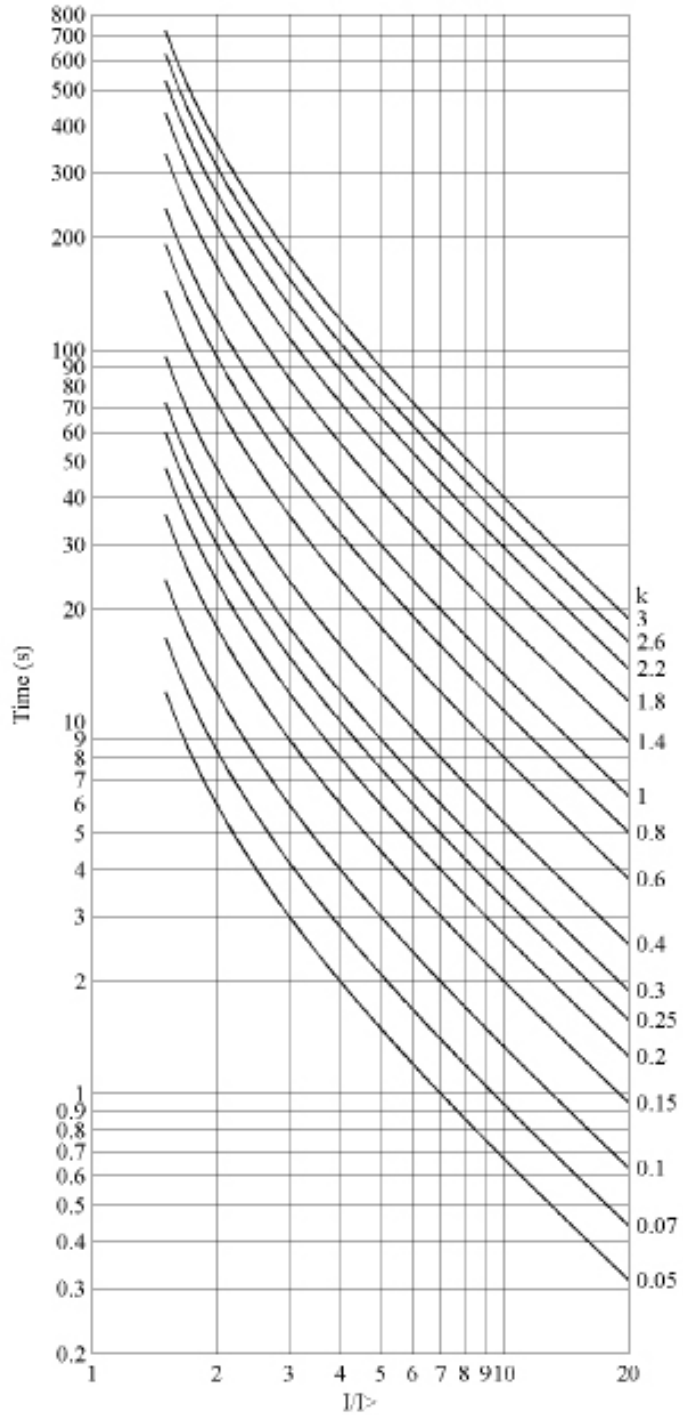


Fig. 6 – Long-time inverse-time characteristics of relay REJ603

### 4.1.8 RI type inverse-time characteristics curve

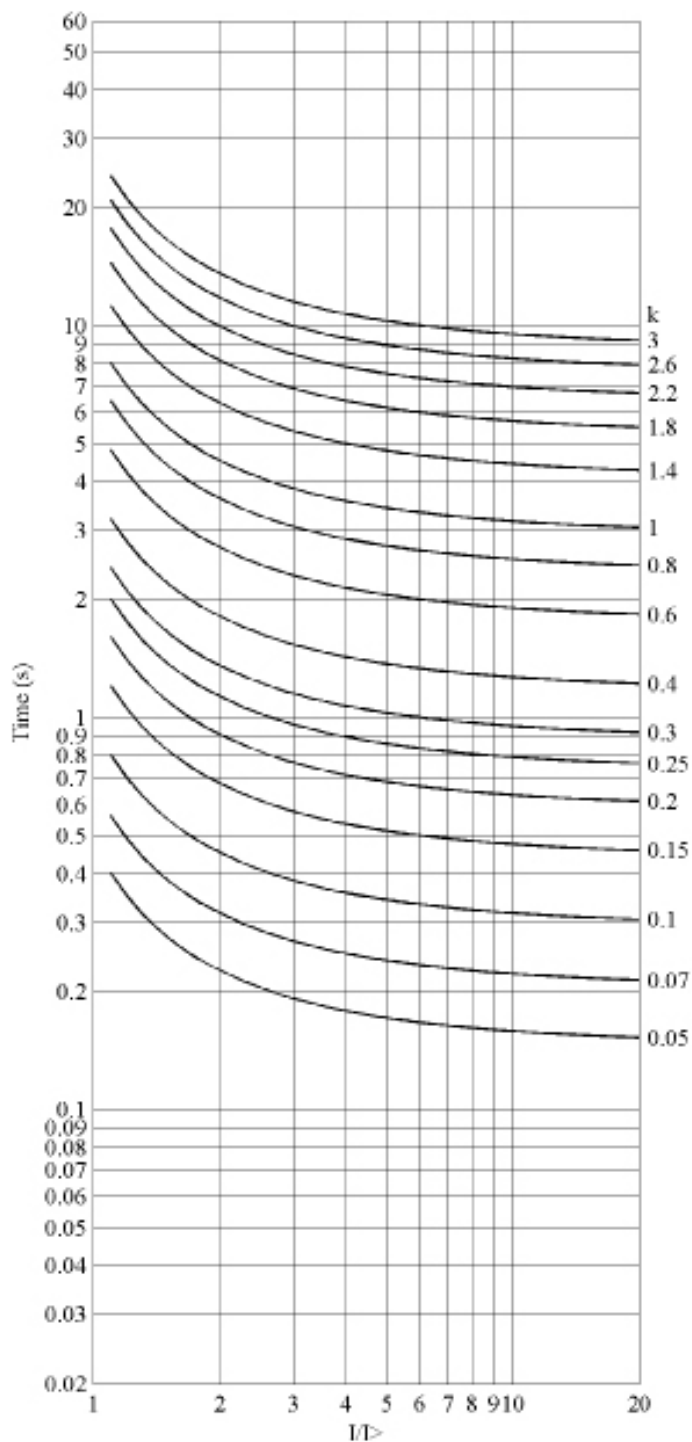


Fig. 7 – RI type inverse-time characteristics of relay REJ603

### 4.1.9 HR Fuse characteristics curve

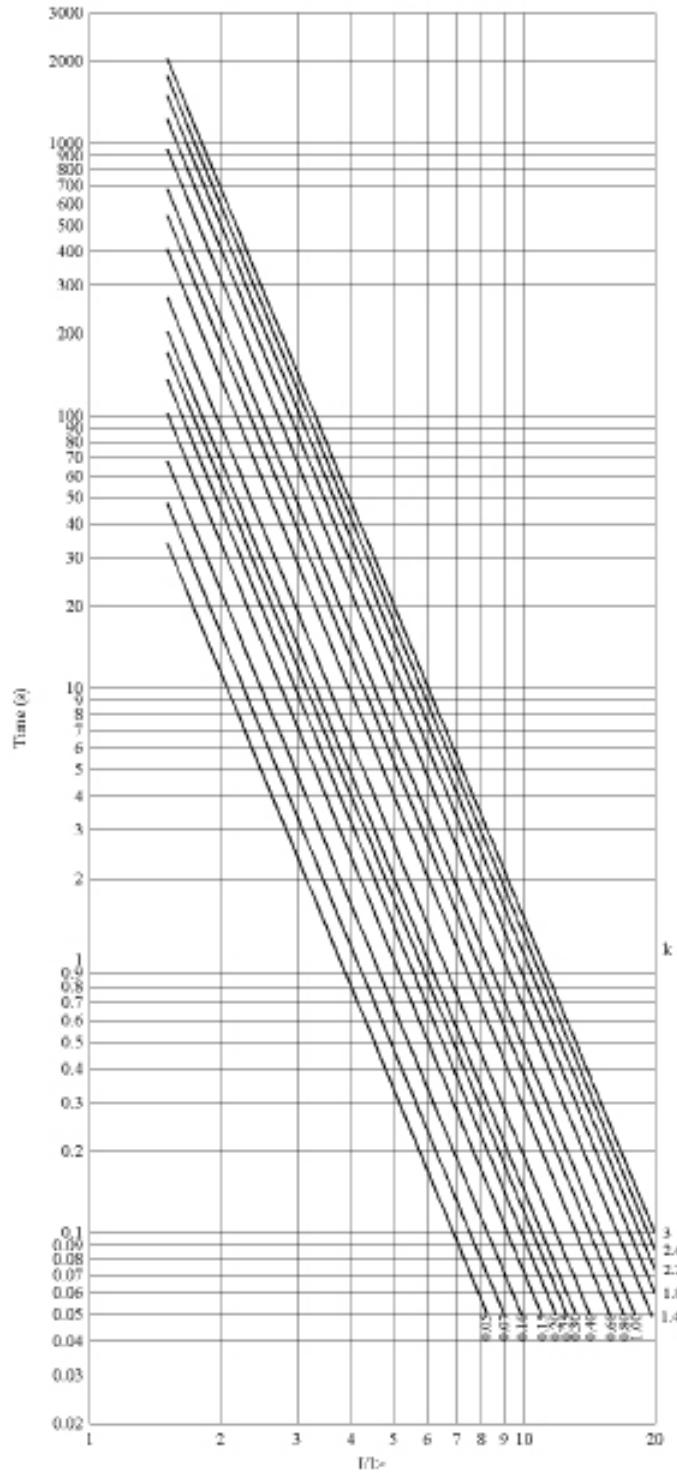


Fig. 8 – HR Fuse characteristics of relay REJ603

### 4.1.10 FR Fuse characteristics curve

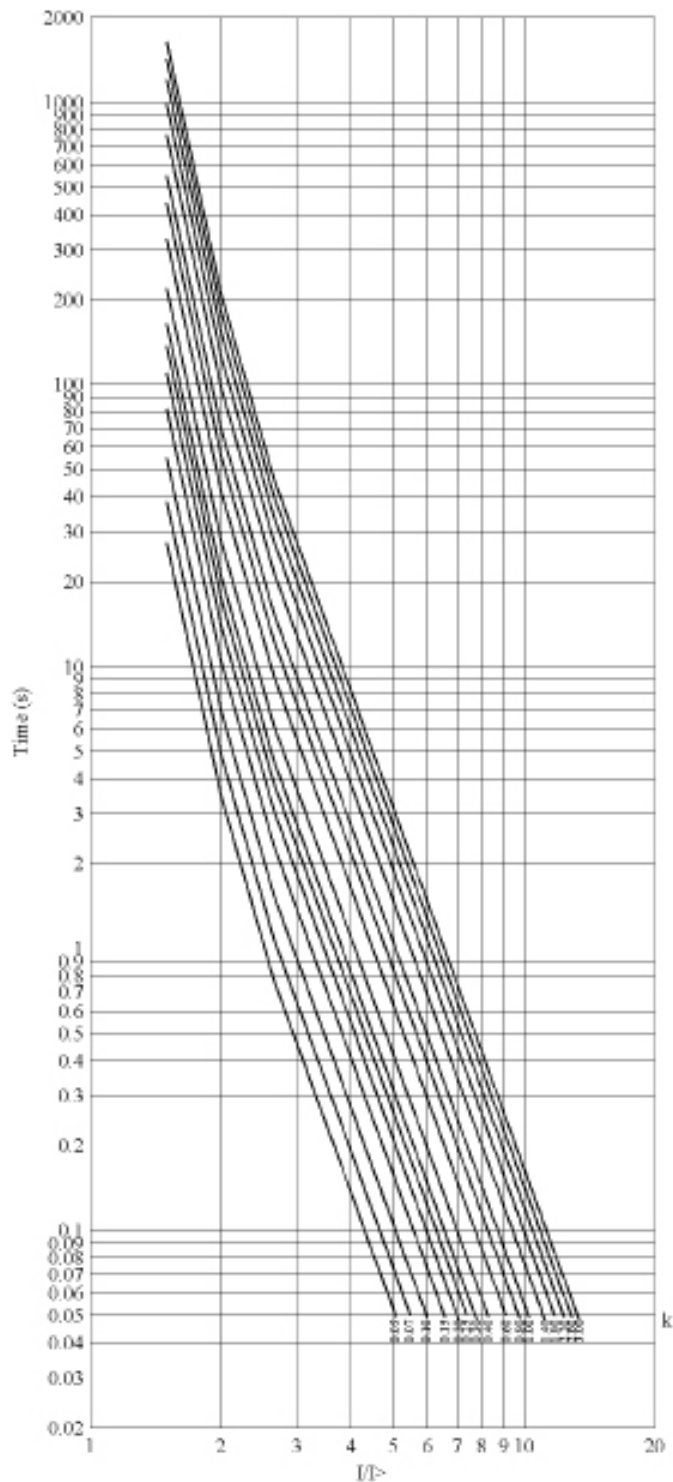


Fig. 9 – FR Fuse characteristics of relay REJ603

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## Section 5      Application Example

### 5.1      Purpose

This application guide presents generally accepted methods of calculation of over current and earth fault relay settings and its time coordination. The following sections detail an individual protection functions in REJ603 relay in addition to where and how they may be applied. Emphasis is given on practical application.

### 5.2      Description

REJ603 is a self-powered numerical relay, primarily used within distribution network. Before proceeding with over current and earth fault relay settings & coordination, the individual load or branch circuit protection should be applied in accordance with local electricity authority. Some of the definitions, which will be used in application example, shall be as below:

#### **Start current:**

It is a minimum value of current at which relay senses the over current and starts its operation. Start current setting is referred as  $I_{>}$ ,  $I_{>>}$ ,  $I_{o>}$ ,  $I_{o>>}$ . Relay must start at the latest when the current exceeds 1.3 times the set start current.

#### **Definite Minimum Time characteristic (DMT):**

During fault condition, relay once starts, operates only after set definite minimum time irrespective of magnitude of fault current. The time settings is referred as  $t_{>}$ ,  $t_{>>}$ ,  $t_{o>}$ ,  $t_{o>>}$ .

#### **Inverse Definite Minimum Time characteristic (IDMT):**

During fault condition, relay once starts; the operating time varies with the magnitude of fault current. Greater the magnitude of fault current lesser is the time of operation depending on the value  $k$ . Suitable characteristics can be selected from the options available in REJ603. Its time multiplier setting is referred as  $k$ ,  $k_o$ .

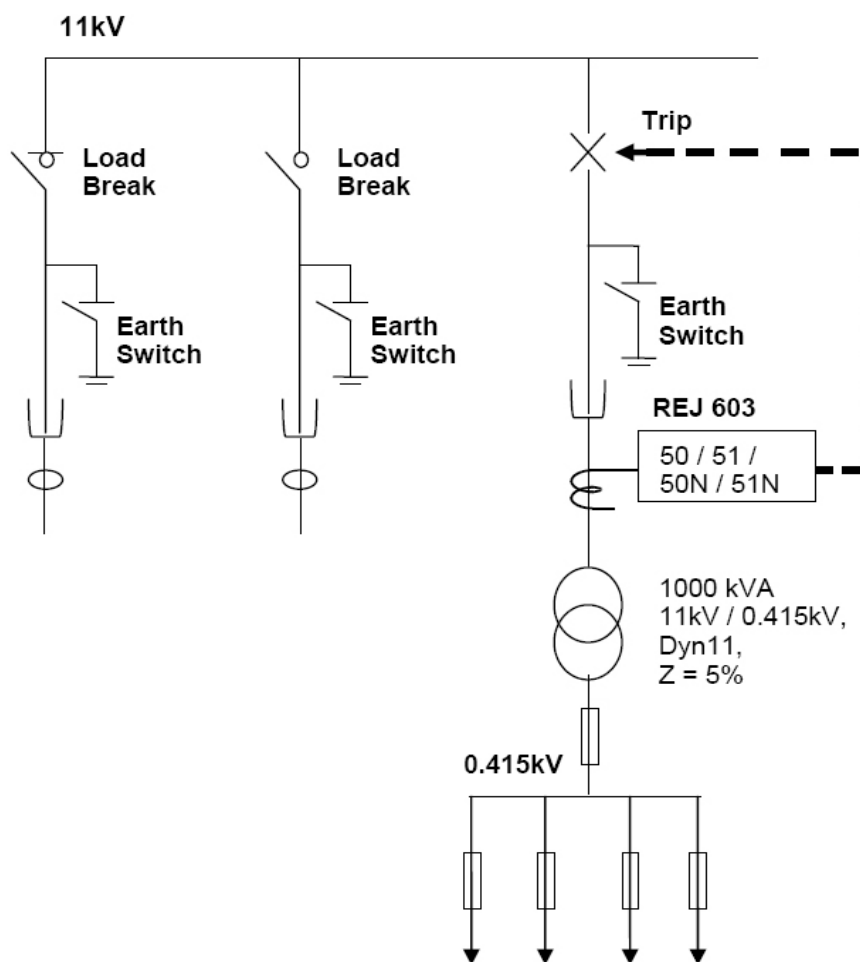


Fig. 10 – Basic circuit diagram of CCV type Ring Main Unit

## 5.3 Setting calculation

### 5.3.1 Selection of CT

Selection of the CT depends on the rated current of the transformer. The same is calculated as shown below:

$$I_N = \frac{S_N}{\sqrt{3} \times U_N}$$

where

$I_N$  = Rated full load current of the power transformer

$S_N$  = Rated power of the power transformer

$U_N$  = Rated phase – phase voltage of the power transformer

Therefore,

$$I_N = \frac{S_N}{\sqrt{3} \cdot U_N} = \frac{1000 \text{ kVA}}{\sqrt{3} \times 11 \text{ kV}} = 52.49 \text{ Amp.}$$

From the measuring CTs table given in technical data, following CT is selected:

CT Type	Range	Current Ratio	$I_{pmin}$ for relay Oprtn.	O/C range	E/F measurement range	
					Internal	External
REJ603 - CT 3	32A – 112A	28.8 / 0.075	28.8 A	28.8A – 2240A	3.2A – 2240A	$0.1 * I_n$ – $20 * I_n$

Setting Range for  $I_s$ :

$I_s$  – 32, 36, 40, 44, 48, 52, 56, 60, 64, 68, 72, 80, 88, 96, 104, 112

REJ603 can measure a short circuit current of a circuit up to 20 times of the highest CT rated current. This means for CT selected above, REJ 603 can measure current up to  $112 \text{ A} \times 20 = 2240 \text{ A}$ .

### 5.3.2

### Fault level calculation

$$\begin{aligned} \text{The three phase fault MVA on } 0.415\text{kV bus is} &= \frac{1000 \text{ kVA}}{\%Z / 100} = \frac{1000 \text{ kVA}}{0.05} \\ &= 20000 \text{ kVA} = 20 \text{ MVA} \end{aligned}$$

The 415kV system is solidly grounded

$$\text{Thus 3 phase fault current on } 0.415\text{kV bus is} = \frac{20}{\sqrt{3} \times 0.415} = 27.83 \text{ kA}$$

$$\text{Reflected 3 phase fault current on } 11 \text{ kV} = \frac{27.83 \text{ kA} \times 0.415 \text{ kV}}{11 \text{ kV}} = 1.049 \text{ kA}$$

Thus with CT 3 (32A-112A) the fault current can be measured clearly by REJ603. Relay can withstand 2.5 x Highest CT rated current continuously and thus care should be taken that continuous load current should be lower than 2.5 x Is i.e. 2.5 x 112 A = 280 Amp.

Now the technical data for relay setting calculation is as follows:

Transformer Technical details: 1 MVA, 11kV, Dyn11, Z = 5%

CT selected is REJ603-CT3 as data indicated earlier.

Relay REJ 603 is used on power transformer 11kV side and is connected to CT 3 secondary with Is selected as 80.

0.415 fault current reflected on 11kV side of the power transformer is 1.049 kA i.e. 1049 Amp.

Consider fault current at 11 kV base as 9 kA.

### 5.3.3 Calculation of setting of high-set O/C

When applying overcurrent protection to the 11kV side of the power transformer it is usual practice to apply a high set instantaneous overcurrent protection (50) in addition to the time delayed low set over current protection (51). Typically this will be set to approximately 1.4 times the reflected 0.415kV fault level such that it will operate only for 11kV side fault. As REJ603 is compliant design against Harmonic distortion and inrush current, this high set overcurrent protection will not operate during transformer energizing condition.

$$\text{Reflected 3 phase fault current on 11 kV} = \frac{27.83 \text{ kA} \times 0.415 \text{ kV}}{11 \text{ kV}} = 1.049 \text{ kA}$$

I>> unit set at = 1.4 x 1049 / 80 = 18.3575

**I>> unit set at 19 x Is i.e. it's primary operating current will be 19 x 80 = 1520 Amp**

I>> unit start current is greater than reflected fault current of 0.415kV on 11Kv and less that fault current at 11kV i.e. 9kAmp,

**Operate time t>> is set at 0.05 Sec.**

High set overcurrent protection will operate instantaneously for fault on 11 kV side of the power transformer wherein fault current is 9 kA and will not operate for the fault on 0.415 kV side of the power transformer.

### 5.3.4 Calculation of setting of low-set O/C

Full load current of the transformer is 52.49 Amp.

Adopted CT Is is 80.

Set I> start current at 1.5 x Transformer full load current.

$$1.5 \times 52.49$$

$$I> \text{ set at } = \frac{\text{-----}}{80} = 0.9841$$

Set I> at 1.0 x Is i.e. it's primary operating current is 1.0 x 80 = 80 Amp.

Primary protection device for fault on 0.415kV is fuse.

Considering the operating time of fuse as 50 mSec. Then REJ 603 acts as back up protection for 0.415 kV fault.

The criteria for assumption of desired operating time depends on the size of the electrical distribution system and location of the protection device.

In this example, desired operating time of low set overcurrent protection (51) is considered as 200 mSec. for fault on 0.415 kV as well as for the fault on 11 kV assuming that the fuse will act as a primary protection for the fault on 0.415 kV side. Thus (51) will act as a backup to fuse provided on 0.415kV and to the ( 50 ) on 11kV .

For fault on 0.415kV :

3 phase fault current of 0.415kV reflected on 11 kV bus = 1049 Amp

$$\text{Fault current} \quad 1049$$

$$\text{With } I> \text{ set at } 1.0 \times I_s, \text{ the PSM} = \frac{\text{-----}}{\text{Primary Operating current} \quad 1 \times 80} = 13.11$$

Thus I / I> = 13.12

Consider Normal Inverse Characteristic :

$$t = \frac{K * \beta}{(I/I_{set})^\alpha - 1}$$

Slope of the time/current curve set	$\alpha$	$\beta$
Normal inverse	0.02	0.14

Operating time at k = 1.0

$$t (s) = \frac{1.0 \times 0.14}{(13.12)^{0.02} - 1} = 2.65 \text{ Sec.}$$

Desired operating time is 0.20 sec and thus k set at 0.08

With k = 0.08, time of operation of I> protection unit is 0.212 sec

Fault on 11 kV :

Considered 3 phase fault current on 11 kV is 9 kAmp

$$\frac{I}{I_{set}} = \frac{9000}{80} = 112.5 \text{ which is greater than } 20.$$

$$I > I_{set} = 80$$

Thus  $I / I_{set} = 20$ .

Operating time for k = 1 is 2.267 sec.

With k = 0.08 , time of operation of I> protection unit is 0.181 Sec.

Thus,

$$I_{set} = 1.0 \times I_s = 1.0 \times 80 = 80 \text{ Amp.}$$

K set at 0.08 with Normal Inverse Characteristic.

### 5.3.5 Calculation of setting of high-set E/F

As the transformer vector group is Dyn11, the single phase earth fault on 0.415kV will not reflect as earth fault on 11 kV delta winding of the transformer.

Single phase to earth fault current in 11kV System is considered as 400 A.

When applying earth fault protection to the 11kV side of the power transformer it is usual practice to apply a high set instantaneous earth fault protection (50N) in addition to the time delayed low set earth fault protection (51N).

I<sub>o>></sub> unit set at 4.0xI<sub>s</sub> i.e. it's primary operating current will be 4.0x80 = 320A

Operate time to>> is set at 0.05 Sec.

High set earth fault protection will operate instantaneously for fault on 11kV side of the power transformer wherein fault current is considered as 400A A.

### 5.3.6 Calculation of setting of high-set E/F

Single phase to earth fault current in 11kV System is considered as 400A.

Adopted CT Is is 80.

Set  $I_{o>}$  at  $1.0 \times I_s$  i.e it's primary operating current is  $1.0 \times 80 = 80$  Amp.

Desired operating time of the low set earth fault protection (51N) is considered as 200 msec for fault on 11 kV. It will be acting as a backup protection for 50N.

For fault on 11 kV:

1 phase fault current on 11 kV bus = 400 A.

$$\text{With } I_{o>} \text{ set at } 1.0 \times I_s, \text{ the PSM} = \frac{\text{Fault current}}{\text{Primary Operating current}} = \frac{400}{1 \times 80} = 5.0$$

Thus  $I / I_{o>} = 5.0$

Consider Normal Inverse Characteristic:

$$t = \frac{K * \beta}{(I / I_{set})^\alpha - 1}$$

Slope of the time/current curve set	$\alpha$	$\beta$
Normal inverse	0.02	0.14

Operating time at  $k = 1.0$

$$t (s) = \frac{1.0 \times 0.14}{(5.0)^{0.02} - 1} = 4.28 \text{ Sec.}$$

Desired operating time is 0.20 Sec. and thus  $k_o$  set at 0.05

With  $k = 0.05$ , time of operation of  $I_{o>}$  protection unit is 0.214 Sec.

Thus,

$I_{o>}$  set at  $1.0 \times I_s = 1.0 \times 80 = 80$  Amp.

K set at 0.05 with Normal Inverse Characteristic.

With  $I_{o>}$  set at  $1.0 \times I_s$ , the PSM =  $\frac{\text{Fault current}}{\text{Primary Operating current}} = \frac{400}{1 \times 80} = 5.0$

Thus  $I / I_s = 5.0$

Consider Normal Inverse Characteristic:

$$t = \frac{K * \beta}{(I/I_{set})^\alpha - 1}$$

Slope of the time/current curve set	$\alpha$	$\beta$
Normal inverse	0.02	0.14

Operating time at  $k = 1.0$

$$t (s) = \frac{1.0 \times 0.14}{(5.0)^{0.02} - 1} = 4.28 \text{ Sec.}$$

Desired operating time is 0.20 Sec. and thus  $k_o$  set at 0.05

With  $k = 0.05$ , time of operation of  $I_{o>}$  protection unit is 0.214 Sec.

Thus,

$I_{o>}$  set at  $1.0 \times I_s = 1.0 \times 80 = 80 \text{ Amp.}$

$K$  set at 0.05 with Normal Inverse Characteristic.

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## Section 6 Relay setting

### 6.1 Setting

The relay settings are done through DIP switches available on the front panel of the relay. The relay is supplied with a factory-set default settings.

### 6.2 Switch setting matrix

The relay setting matrix is available on the terminal side of the relay and the same is explained below. There are six, 8-pole DIP switches on the front panel. The setting is done by adjusting these switches corresponding to the setting matrix/ table.

Descript of parameter	Switch block	Switch number
Rated CT current	S1	1-4
Earth fault measurement	S1	5
t> / k selection	S2	1-4
to> / k selection	S2	5-8
I> selection	S3	1-5
Characteristic selection for Phase O/C	S3	6-8
Io> selection	S4	1-4
Characteristic selection for Earth E/F	S4	6-8
I>> selection	S5	1-4
t>> selection	S5	5-8
Io>> selection	S6	1-4
to>> selection	S6	5-8

## 6.2.1 Rated CT and earth current measurement selection

The rated CT current,  $I_s$  is set by adjusting the switch S1/ 1-4

S1-1	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S1-2	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S1-3	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
S1-4	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON	ON
CT1	8	9	10	11	12	13	14	15	16	17	18	20	22	24	26	28
CT2	16	18	20	22	24	26	28	30	32	34	36	40	44	48	52	56
CT3	32	36	40	44	48	52	56	60	64	68	72	80	88	96	104	112
CT4	64	72	80	88	96	104	112	120	128	136	144	160	176	192	208	224
CT5	128	144	160	176	192	208	224	240	256	272	288	320	352	384	416	448

Earth current measurement: The internal or external CT is selected by switch S1/ 5

S1, 5	OFF	ON
Earth fault measurement	by internal calculation	by external input

In addition to DIP switches the fine setting can be done through the add-on HMI module if available. Setting switch S1/ 6 can use this feature.

## 6.2.2 Operation time selection for low-set overcurrent and earth-fault

$t_{> / K}$  selection, switch S2/ 1-4

S2-1	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S2-2	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S2-3	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
S2-4	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON	ON
$t_{> / k}$	0.05	0.07	0.1	0.15	0.2	0.25	0.3	0.4	0.6	0.8	1	1.4	1.8	2.2	2.6	3

$t_{> / k}$  selection, switch S2/ 5-8

S2-5	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S2-6	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S2-7	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
S2-8	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON	ON
$t_{> / k_0}$	0.05	0.07	0.1	0.15	0.2	0.25	0.3	0.4	0.6	0.8	1	1.4	1.8	2.2	2.6	3

## 6.2.3 Operation characteristic / start current selection for low-set overcurrent

### I > selection, switch S3/ 1-5

S3-1	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S3-2	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S3-3	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
S3-4	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON	ON
S3-5*	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF
S3-5**	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON
I>*	0.9	0.95	1	1.05	1.1	1.15	1.2	1.25	1.3	1.35	1.4	1.45	1.5	1.55	1.6	1.65
I>**	1.7	1.75	1.8	1.85	1.9	1.95	2	2.05	2.1	2.15	2.2	2.25	2.3	2.4	2.5	E

### CI - characteristic curve selection for phase, switch S3/ 6-8

S3-6	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S3-7	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S3-8	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
CP	DMT	NI	EI	VI	LI	RI	HR	FR	NA	NA	NA	NA	NA	NA	NA	NA

## 6.2.4 Operation characteristic / start current selection for low-set earth-fault

### I<sub>0</sub>> selection, switch S4/ 1-4

S4-1	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S4-2	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S4-3	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
S4-4	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON	ON
S4-5*	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF
S4-5**	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON
I <sub>0</sub> > *	0.1	0.125	0.15	0.175	0.2	0.225	0.25	0.275	0.3	0.325	0.35	0.375	0.4	0.425	0.45	0.475
I <sub>0</sub> > **	0.5	0.525	0.575	0.6	0.625	0.65	0.675	0.7	0.725	0.75	0.8	0.85	0.9	0.95	1	E

### CE - characteristic curve selection for earth, switch S4/ 6-8

S4-6	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S4-7	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S4-8	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
CE	DMT	NI	EI	VI	LI	RI	HR	FR	NA	NA	NA	NA	NA	NA	NA	NA

## 6.2.5 Operation time / start current selection for high-set overcurrent

l>> selection, switch S5/ 1-4

S5-1	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S5-2	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S5-3	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
S5-4	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON	ON
l>>	1	2	3	4	5	6	7	8	9	10	12	14	16	18	20	E

t>> selection, switch S5/ 5-8

S5-5	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S5-6	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S5-7	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
S5-8	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON	ON
t>>	0.04	0.07	0.1	0.15	0.2	0.25	0.3	0.4	0.6	0.8	1	1.4	1.8	2.2	2.6	3

## 6.2.6 Operation time / start current selection for low-set overcurrent

lo>> selection, switch S6/ 1-4

S6-1	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S6-2	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S6-3	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
S6-4	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON	ON
lo>>	1	2	3	4	5	6	7	8	9	10	12	14	16	18	20	E

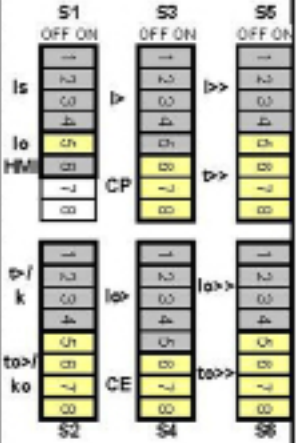
to>> selection, switch S6/ 5-8

S6-5	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON
S6-6	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON
S6-7	OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	OFF	ON	ON	ON	ON
S6-8	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON	ON
to>>	0.04	0.07	0.1	0.15	0.2	0.25	0.3	0.4	0.6	0.8	1	1.4	1.8	2.2	2.6	3

### 6.3 Total Switch setting matrix

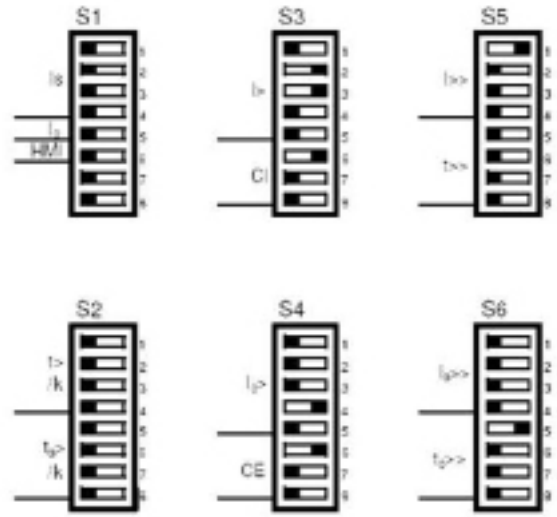
The REJ603 relay on the terminal side contains below indicated setting matrix view, for ease of setting the relay.

DIP I		OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON	OFF	ON		
DIP II		OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	OFF	ON	ON	OFF	ON		
DIP III		OFF	OFF	OFF	OFF	ON	ON	ON	ON	OFF	OFF	OFF	ON	ON	ON		
DIP IV		OFF	OFF	OFF	OFF	OFF	OFF	OFF	ON	ON	ON	ON	ON	ON	ON		
DIP v*		OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF	OFF		
DIP v**		ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON	ON		
I <sub>s</sub>	S1 / 1-4																
CT1		8	9	10	11	12	13	14	15	16	17	18	20	22	24	26	28
CT2		16	18	20	22	24	26	28	30	32	34	36	40	44	48	52	56
CT3		32	36	40	44	48	52	56	60	64	68	72	80	88	96	104	112
CT4		64	72	80	88	96	104	112	120	128	136	144	160	176	192	208	224
CT5		128	144	160	176	192	208	224	240	256	272	288	320	352	384	416	448
I <sub>o</sub>	S1 / 5	OFF = Earthfault measurement by internal calculation								ON = Earthfault measurement by external input							
HMI	S1 / 6	OFF = Settings by DIP switches								ON = Settings by DIP switches (coarse) + HMI (fine)							
Spare	S1 / 7-8																
t <sub>&gt;/k</sub>	S2 / 1-4	0.05	0.07	0.1	0.15	0.2	0.25	0.3	0.4	0.6	0.8	1	1.4	1.8	2.2	2.6	3
I <sub>o&gt;/k<sub>o</sub></sub>	S2 / 5-8	0.05	0.07	0.1	0.15	0.2	0.25	0.3	0.4	0.6	0.8	1	1.4	1.8	2.2	2.6	3
I <sub>&gt;*</sub>	S3 / 1-5	0.9	0.95	1	1.05	1.1	1.15	1.2	1.25	1.3	1.35	1.4	1.45	1.5	1.55	1.6	1.65
I <sub>&gt;**</sub>	S3 / 1-5	1.7	1.75	1.8	1.85	1.9	1.95	2	2.05	2.1	2.15	2.2	2.25	2.3	2.4	2.5	E
CI	S3 / 6-8	DMT	NI	SI	VI	LI	RI	HR	FR	NA	NA	NA	NA	NA	NA	NA	NA
I <sub>o&gt;*</sub>	S4 / 1-5	0.1	0.125	0.15	0.175	0.2	0.225	0.25	0.275	0.3	0.325	0.35	0.375	0.4	0.425	0.45	0.475
I <sub>o&gt;**</sub>	S4 / 1-5	0.5	0.525	0.575	0.6	0.625	0.65	0.675	0.7	0.725	0.75	0.8	0.85	0.9	0.95	1	E
CE	S4 / 6-8	DMT	NI	SI	VI	LI	RI	HR	FR	NA	NA	NA	NA	NA	NA	NA	NA
I <sub>o&gt;</sub>	S5 / 1-4	1	2	3	4	5	6	7	8	9	10	12	14	16	18	20	E
t <sub>&gt;&gt;</sub>	S5 / 5-8	0.04	0.07	0.1	0.15	0.2	0.25	0.3	0.4	0.6	0.8	1	1.4	1.8	2.2	2.6	3
I <sub>o&gt;&gt;</sub>	S6 / 1-4	1	2	3	4	5	6	7	8	9	10	12	14	16	18	20	E
t <sub>o&gt;&gt;</sub>	S6 / 5-8	0.04	0.07	0.1	0.15	0.2	0.25	0.3	0.4	0.6	0.8	1	1.4	1.8	2.2	2.6	3



### 6.4 Switch setting matrix example

Selection of I<sub>s</sub> based ON CT, I<sub>s</sub> = 32 for CT 3  
 Earth measurement: Internal  
 HMI selection: DIP switches  
 I<sub>></sub> = 120% or 1.2  
 CI = NI – Normal inverse  
 t<sub>>/k</sub> = 0.05  
 I<sub>o></sub> = 30% or 0.3  
 CE = NI  
 t<sub>o>/k</sub> = 0.05  
 I<sub>o>></sub> = 200% or 2  
 t<sub>>></sub> = 0.04  
 I<sub>o>></sub> = 100%, 1  
 t<sub>o>></sub> = 0.07



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## Section 7 Installation and commissioning

### 7.1 Unpacking and inspecting the device

REJ603 products, although of robust construction, require careful handling prior to installation on site. The delivered products should always be examined to ensure that no damage has been sustained during transit.

Remove transport packing carefully without force. Appropriate tools needs to be used.

Check the relay for transport damages. If the product has been damaged, a claim should be made to the transport contractor and the local representative of ABB should be promptly notified. Compare the type designation of the product with the ordering information to verify that you have received the right product.

Electrostatic discharge (ESD)

The products contain components that are sensitive to electrostatic discharge. The electronic circuits are well protected by the relay case and therefore the rear panel may not be removed.

### 7.2 Storage

On receipt, the apparatus must be carefully unpacked and checked as described under chap. 7.1. Should installation not be carried out immediately, the apparatus must be repacked using the original packing material. Should the original packing material no longer be available, store the apparatus in a dry, dust-free, covered area which is non corrosive and has a temperature of between – 40 °C and + 85 °C.

## 7.3 Checking environmental conditions and mounting space

The mechanical and electrical environmental conditions at the installation site must be within the limits described in the technical data.

- Avoid installation in dusty, damp places.  
Avoid places susceptible to rapid temperature variations, powerful vibrations and shocks, surge voltages of high amplitude and fast rise time, strong induced magnetic fields or similar extreme conditions.
- Check that sufficient space is available.  
To allow access for maintenance and future modifications a sufficient space is needed in front and at side of the relay.
- Suitably qualified personnel with adequate knowledge of the apparatus must carry out all the installation operations.
- The relay should be disconnected before carrying out any work on relay.

## 7.4 Mounting the relay

The relay is has provision of wall mounting.

The space requirement of mounting:

Dimensions (H x W x D): . . . . . 160x96x149mm

Weight: . . . . . 800g

By using the six nos. 4 mm drill holes, the relay is directly mounted on to the mounting plate. Detailed mounting drawing with all measurement is furnished in section 7.6.

## 7.5 Relay wiring

The connection wiring to the relay should be made by using single strand wire or stranded wire with the use of insulated crimp terminal to maintain the insulation requirements. The wire with below indicated cross-section should be used for wiring:

- .0.2 - 2.5 sq. mm single-core
- .0.2 - 2.5 sq. mm finely stranded

## 7.6 Relay mounting dimensions

The relay is projection mounted. The relay provides IP54 on the front side. The overall dimensions of the relay are as follows:

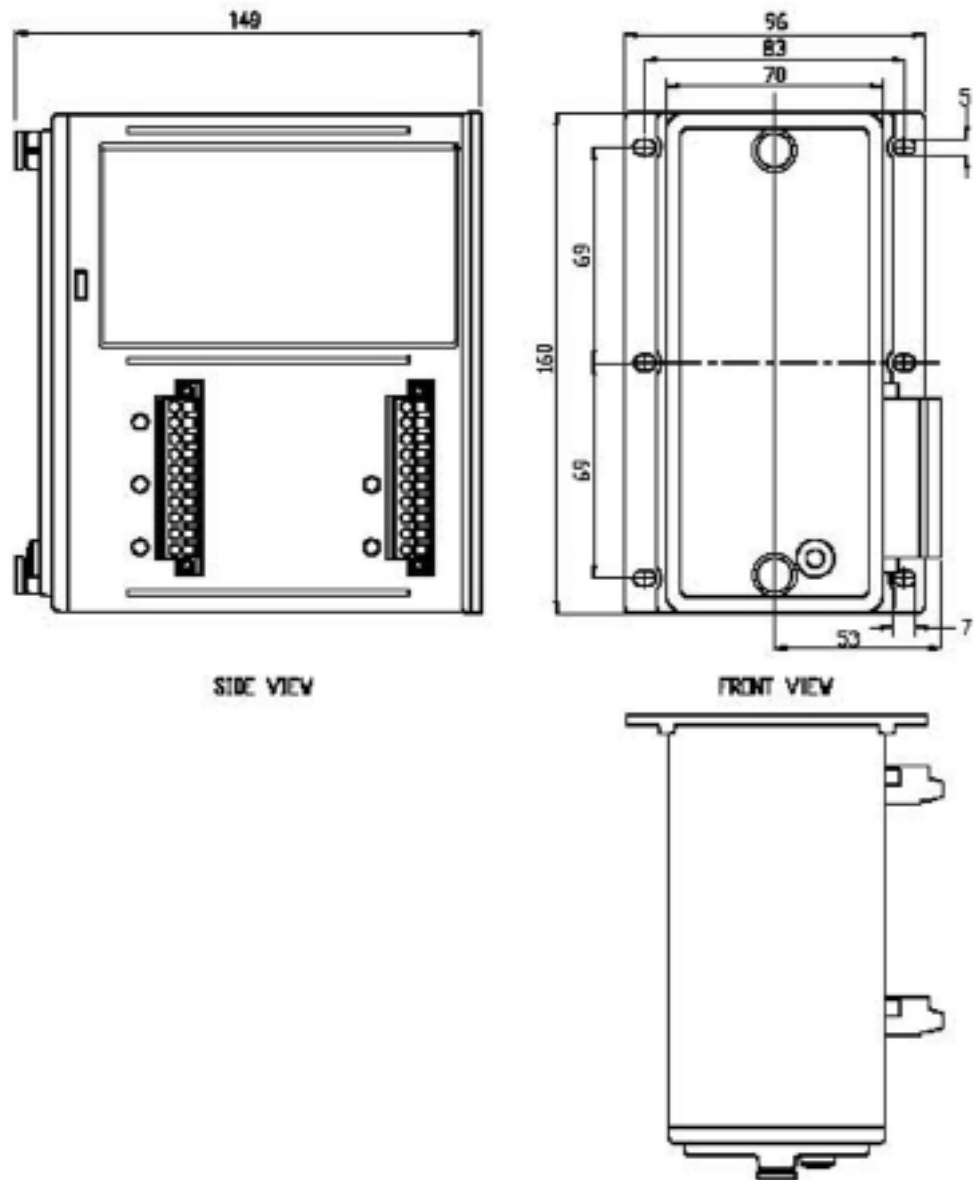


Fig. 4 – Relay mounting dimensions

## 7.7 Relay connection diagram

The relay is projection mounted. The relay provides IP54 on the front side. The overall dimensions of the relay are as follows:

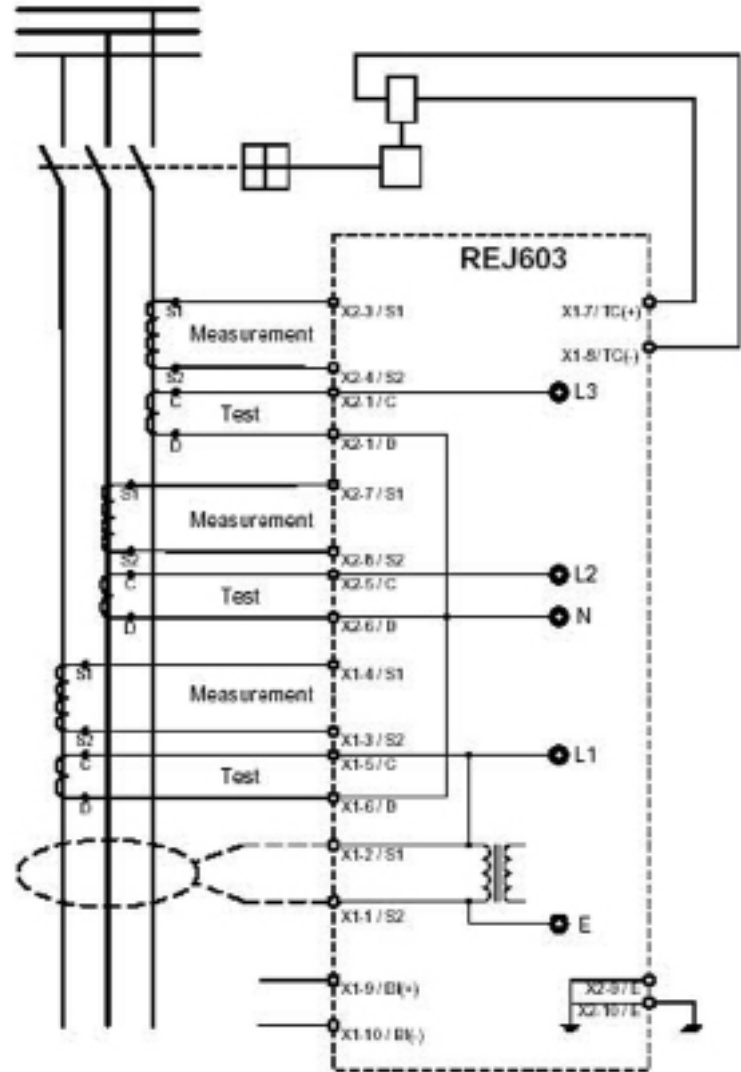


Fig. 5 – Relay connection diagram

## 7.8 Relay connection

The relay is available with three analogue phase measuring inputs. The special CTs are designed for REJ603 relay, the current measuring inputs of the relay are specially adjusted to these CTs. The details of these CTs are available in technical data section 3. The relay can be powered from these three analogue phase measuring inputs as indicated below:

- .CT input phase L1 (S1, S2), Terminal no. X1.3, X1.4
- .CT input phase L2 (S1, S2), Terminal no. X2.7, X2.8
- .CT input phase L3 (S1, S2), Terminal no. X2.3, X2.4

The earth current is calculated from the three currents.

Alternatively additional earth current measuring input is available in relay for connection of core balance current transformer (CBCT) if needed which can be connected to below indicated input:

- .CT input earth L1 (S1, S2), Terminal no. X1.2, X1.1

The special CTs for REJ603 have a test windings to simulate primary current, test socket are provided on the relay through which current can be injected in the test winding of CT's which facilitates the testing of complete protection scheme including CT, relay and trip coil.

- .Test socket - L1, L2, L3, N for phase circuit testing
- .Test socket - L1, E. for earth circuit testing

Galvanically isolated binary input is provided with a wide input voltage range 24-240V AC/DC for wiring external trip signal to trip circuit breaker.

- .Binary input BI(+), BI(-), Terminal no. X1.9, X1.10

Low energy impulse type trip output is available to trip circuit breaker.

- .Trip Input TC(+), TC(-), Terminal no. X1.7, X1.8

Earthling should be connected to earth terminal

- .Earth Input, Terminal no. X2.9, X2.10

On the front of the relay, LED indications for Unit ready and relay internal fault are available.

Phase and earth over current fault indication are provided through manually re-settable mechanical Flag which ensures availability of relay operation indication even in absence of the primary CT current.

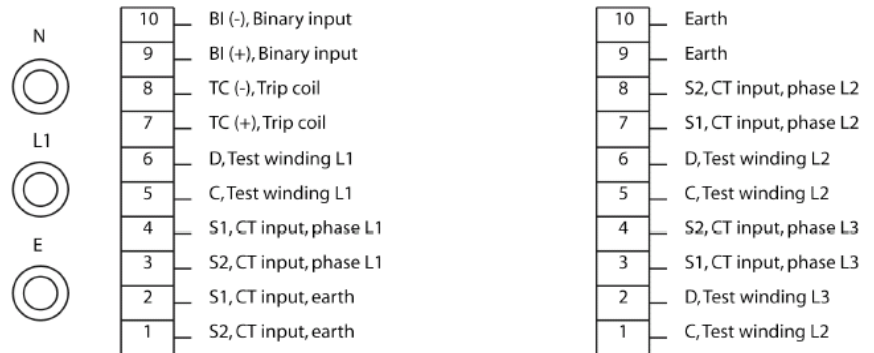


Fig. 6 – Terminal arrangement diagram

Important points to be taken in to consideration during wiring and operation:

- . No winding terminal of the measuring winding of CT to be earthed. Earthling is done internally and brought out at earth terminal.
- . The secondary side of test winding always to be kept open (except when relays are tested)
- . Polarity of tripping coil wiring TC(+) and TC(-) needs to be properly checked to have correct tripping operation.

## 7.9 Relay commissioning

During the first time commissioning the relay, it is necessary for user to become familiar with the method by which the settings are applied. All the settings of relay can be changed by using DIP switches refer section 6.

The customer shall be responsible for determining the application-specific settings applied to the relay and for testing of any scheme logic applied by external wiring.

### Minimum equipment required:

- . Current injection test set.
- . Multimeter with suitable ac current range.
- . Multimeter with recording of maximum value of dc voltage (for dc amplitude of pulse tripping measuring)
- . Continuity tester

### Pre-commissioning checks:

Below indicated pre-commissioning checks are generally done before commissioning

- . Visual inspection
- . Wiring checking
- . Insulation resistance checking

### Testing of the relay:

After installation and before putting into operation complete in and out (from CT to trip coil function) can be checked with use of test winding which gives the possibility of injecting the simulated primary current.

For testing, secondary testing system with 1A rated output current is required. The test current is fed through sockets L1, L2, L3 and N available beside the connection terminal on the relay. The test winding is rated such that the fed current of 1A balances a primary current of 50A (CT type CT2- 16A-56A). Applying the 1A rated current and connecting trip coil at output with setting of relay kept to minimal values, a complete check of protection system is possible with the tripping circuit. Connection diagram for testing of relay with test winding is given in figure 5.

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By injecting 1A rated current in test winding, gives the possibility of simulated primary current injection. The value of simulated primary current depends on Primary CT used, details given below:

<b>CT Type</b>	<b>Current applied to Test winding</b>	<b>Simulated Primacy Current</b>
CT2: 16A–56A	1A	50A
CT3: 32A–112A	1A	100A
CT4: 64A–224A	1A	200A
CT5: 128A–448A	1A	400A

This functionality is quite helpful during commissioning and periodic health check of relay.

## 7.10

### Relay ordering information

The relay is available in single variant. The ordering code of the relay is as below:

Order Code: REJ603BBB10NN3XA

Specific ring phase CT's needs to be used along with the relays. The ordering details for the same can be available from CT data sheet no. 1YMA583791R0001-4.





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